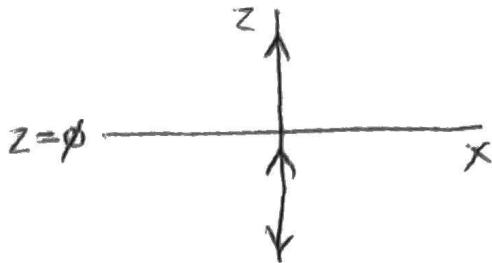


# HW #4 Solutions

## Reflection/Transmission - 4

1)

$$\vec{E} = E_0 e^{i(kz-\omega t)} \hat{x}$$



$$\vec{E}'' = E_0'' e^{-i(kz+\omega t)} (\cos\theta \hat{x} + \sin\theta \hat{y}) \quad \text{BCs evaluated at } z=\phi, t=\phi$$

$$\vec{E}' = E_0' e^{i(kz-\omega t)} (\cos\phi \hat{x} + \sin\phi \hat{y})$$

$\vec{E}' \times \hat{n} = \phi$  — tangential components of  $\vec{E}$  are continuous

$$E_0 \hat{x} + E_0'' \cos\theta \hat{x} + E_0'' \sin\theta \hat{y} = E_0' \cos\phi \hat{x} + E_0' \sin\phi \hat{y} \quad ①$$

$\vec{H} \times n = \phi$  — tangential components of  $\vec{H}$  are continuous

~~$$\vec{H} = \frac{1}{\mu} \vec{k} \times \vec{E} \text{ so } \vec{H} = \frac{1}{\mu} \vec{k} \times \vec{E}$$~~

w's can be ignored — all the same

$$\frac{1}{\mu} K E_0 (\hat{z} \times \hat{x}) + \frac{1}{\mu} K E_0'' (-\hat{z} \times \hat{x} \cos\theta + (\hat{z} \times \hat{y} \sin\theta)) = \frac{1}{\mu} K' E_0' (\cos\phi \hat{z} \times \hat{x} + \sin\phi \hat{z} \times \hat{y}) \quad ②$$

from ①  $\hat{y}$  ( $E_0'' \sin\theta = E_0' \sin\phi$ )

②  $\hat{x}$  ( $\frac{1}{\mu} K E_0'' \sin\theta = -\frac{1}{\mu} K' E_0' \sin\phi$ )

so  $\sin\theta / \sin\phi = \frac{E_0'}{E_0''} = -\frac{E_0'}{E_0''} \frac{K'}{K} \frac{\mu}{\mu'} - \text{not possible}$   
unless  $\phi = \theta = \phi$

$\hat{x}$  terms in ①,  $\hat{y}$  terms in ② not needed for argument

from class  $\frac{E_0'}{E_0} = \frac{2n}{n+n'} \quad , \quad \frac{E_0''}{E_0} = \frac{n-n'}{n+n'}$

$$\langle S \rangle = \langle U \rangle V = \frac{1}{2} \epsilon E^2 \frac{1}{\sqrt{\mu \epsilon}} = \frac{1}{2} \sqrt{\epsilon} E^2 \quad n = \frac{\epsilon}{V} = C \sqrt{\mu \epsilon}$$

$$\langle S \rangle = \frac{1}{2} \frac{n}{c \mu} E^2 \quad \sqrt{\epsilon} = \frac{n}{c \sqrt{\mu}}$$

$$\frac{\langle S \rangle_R}{\langle S \rangle_I} = \frac{\langle S'' \rangle}{\langle S \rangle} = \frac{\gamma_2 n / c \mu \left( \frac{n-n'}{n+n'} \right)^2 E_0^2}{\gamma_2 n / c \mu E_0^2} = \left( \frac{n-n'}{n+n'} \right)^2 = \frac{1}{2}$$

$$\text{so } n-n' = \pm \frac{1}{\sqrt{2}} (n+n') \quad n \left( 1 \mp \frac{1}{\sqrt{2}} \right) = n' \left( 1 \pm \frac{1}{\sqrt{2}} \right)$$

$$\frac{n}{n'} = \frac{(\sqrt{2} \pm 1) / \sqrt{2}}{(\sqrt{2} \mp 1) / \sqrt{2}} = \frac{\sqrt{2} \pm 1}{\sqrt{2} \mp 1} = 5.83 \text{ and } .172$$

these are inverses of each other

so  $\frac{1}{2}$  is reflected,  $\frac{1}{2}$  is transmitted for light incident from either side of the interface

you can check by transmitted fraction is also  $\frac{1}{2}$

## Reflection/Transmission - f2

### Energy Conservation

$$\langle \vec{S} \rangle = \langle U \rangle \hat{V} \hat{k}$$

$$= \frac{1}{2} \sqrt{\epsilon} E_0^2 \hat{k}$$

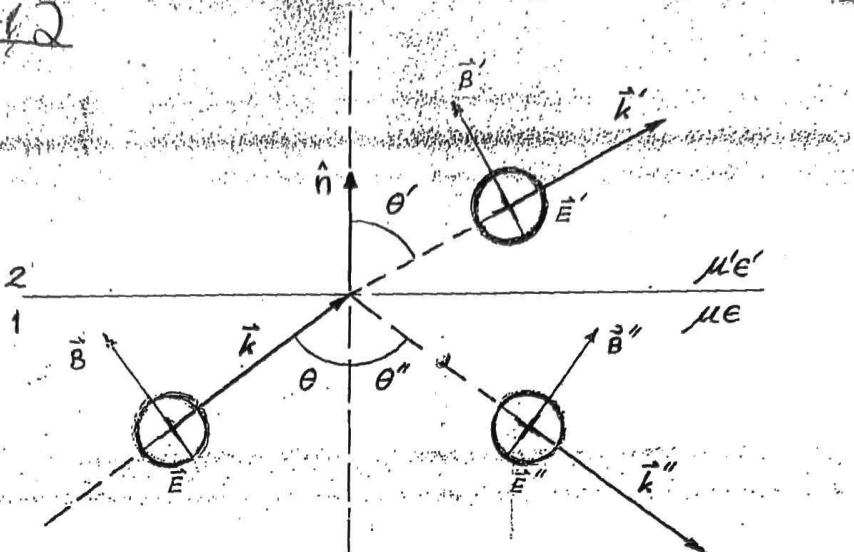
$$v = \frac{c}{n} = \frac{1}{\sqrt{\mu \epsilon}}$$

$$\text{so } n = c \sqrt{\mu \epsilon} \text{ so}$$

$$\langle \vec{S} \rangle = \frac{1}{2} \frac{n}{\mu c} E_0^2 \hat{k}$$

$$|\vec{S} \cdot \hat{n}| = |S' \cdot \hat{n}| + |S'' \cdot \hat{n}|$$

Ignore  $\frac{1}{2}$ ,  $\mu$ , and  $c$  in  $\vec{S}$



$$\vec{E} \parallel (\hat{n} \times \vec{k})$$

$\vec{E}_\perp$  case

$$\frac{E_0'}{E_0} = \frac{2n \cos \theta}{n \cos \theta + \frac{\mu}{\mu'} \sqrt{n'^2 - n^2 \sin^2 \theta}} = \frac{2n \cos \theta}{a + b}$$

$$\frac{E_0''}{E_0} = \frac{a - b}{a + b} \quad \mu = \mu'$$

$$n E_0^2 \cos \theta = n \left( \frac{a - b}{a + b} \right)^2 \cos \theta E_0^2 + n' \frac{4n^2 \cos^2 \theta}{(a + b)^2} E_0^2 \cos \theta' \quad \text{cancel } n, E_0^2, \cos \theta$$

$$(a + b)^2 = (a - b)^2 + 4n n' \cos \theta \cos \theta'$$

$$a^2 + 2ab + b^2 = a^2 - 2ab + b^2 + 4n n' \cos \theta \cos \theta' \quad 4ab = 4n n' \cos \theta \cos \theta'$$

$$b = \sqrt{n'^2 - n^2 \sin^2 \theta} = \sqrt{n'^2 - n'^2 \sin^2 \theta'} = n' \sqrt{1 - \sin^2 \theta'} = n' \cos \theta'$$

$$n \cos \theta (n' \cos \theta') = n n' \cos \theta \cos \theta' \quad \checkmark$$

Wangness 25-3

$$\tan \theta_p = \frac{n_2}{n_1} \quad \sin \theta_c = \frac{n_2}{n_1}$$

so we need to prove that  $\theta_p - \theta_c < \phi$

$$\text{or } \tan^{-1} \frac{n_2}{n_1} - \sin^{-1} \frac{n_2}{n_1} < \phi \quad \tan^{-1} \frac{n_2}{n_1} < \sin^{-1} \frac{n_2}{n_1}$$

now take tan of both sides

$$\begin{aligned} "y" &= n_2 \\ "r" &= n_1 \end{aligned} \quad \text{so } "x" = \sqrt{n_1^2 - n_2^2}$$

$$\frac{n_2}{n_1} < \frac{n_2}{\sqrt{n_1^2 - n_2^2}}$$

so yes  $\theta_p < \theta_c$

so as you increase  $\theta$  from  $0^\circ$ , you reach the angle at which the reflected light is completely polarized  $\perp$  to the plane of incidence before you reach the angle  $\phi$  that results in total internal reflection

$$n_2/n_1 = .75 \implies \theta_p = 36.9^\circ, \theta_c = 48.6^\circ$$

$$.5 \quad \theta_p = 26.6^\circ, \theta_c = 30^\circ$$

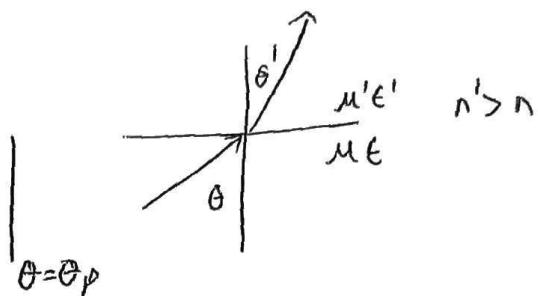
$$.25 \quad \theta_p = 14.0^\circ, \theta_c = 14.5^\circ$$

as  $\theta_p \rightarrow 0^\circ$ ,  $\theta_c \rightarrow \theta_p$  (since  $\sin \theta \approx \tan \theta \approx \theta$ )  
 $(n_1 \gg n_2)$

## Reflection/Transmission - I

At Brewster angle,  $\mu = \mu'$

$$\text{i) } \frac{E_0'}{E_0} = \frac{2nn' \cos \theta}{\tan \theta + n' \cos \theta + n \sqrt{n'^2 - n^2 \sin^2 \theta}}$$



∴ by  $\cos \theta_p$

$$\frac{E_0'}{E_0} = \frac{2nn'}{n'^2 + n \sqrt{\frac{n'^2 - n^2 \sin^2 \theta}{\cos^2 \theta}}} = \frac{2nn'}{n'^2 + n \sqrt{\frac{n'^2}{\cos^2 \theta} - n^2 \frac{n'^2}{n^2}}}$$

$$= \frac{2nn'}{n'^2 + nn' \sqrt{\frac{1 - \cos^2 \theta}{\cos^2 \theta}}} = \frac{2nn'}{n'^2 + nn' \tan \theta_p} = \frac{2nn'}{n'^2 + nn' n'/n} = \frac{2nn'}{2n'^2}$$

$$\rightarrow \boxed{\frac{E_0'}{E_0} = \frac{n}{n'}}$$

i)  $\langle U \rangle = \frac{1}{2} \epsilon E_0^2$

b)  $U = \frac{1}{2} \epsilon E_0^2 \quad U' = \frac{1}{2} \epsilon' \frac{n^2}{n'^2} E_0^2$

$$n = \frac{c}{v} = c \sqrt{\mu \epsilon}$$

$$\text{so } n^2 \propto \epsilon$$

$$\text{so } U = \frac{1}{2} n^2 E_0^2, \quad U' = \frac{1}{2} n'^2 \frac{n^2}{n'^2} E_0^2 = \frac{1}{2} n^2 E_0^2 \checkmark$$

so both waves have the same energy density even though the electric fields have different magnitudes

c)  $\langle S \rangle = \langle U \rangle V$  so definitely not.  $V \propto \frac{1}{n}$

the energy densities are the same but the energy is transported at different rates and also in different directions

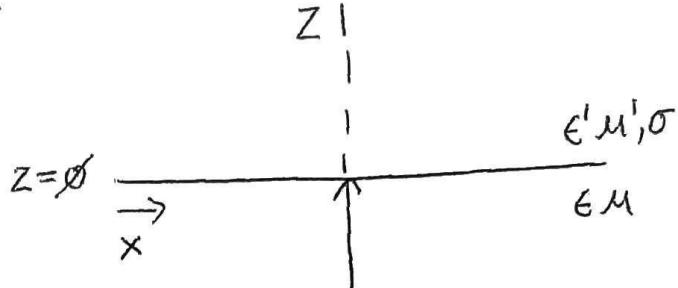
$$\text{so } \frac{|S'|}{|S|} = \frac{\frac{1}{2} n^2 E_0^2 \frac{1}{n'}}{\frac{1}{2} n^2 E_0^2 \frac{1}{n^2}} = \frac{n}{n'} \checkmark$$

## Reflection/Transmission - 3

a)

$$\vec{E} = E_0 e^{i(kz-wt)} \hat{x}$$

$$\vec{E}'' = -E_0 e^{-i(kz+wt)} \hat{x}$$



$$\vec{E}_{\text{total}} = \vec{E} + \vec{E}'' = E_0 \hat{x} \left( e^{i(kz-wt)} + e^{-i(kz+wt)} \right)$$

$$= E_0 \hat{x} \left[ \cos(kz-wt) + \cos(kz+wt) + i(\sin(kz-wt) + \sin(kz+wt)) \right]$$

$$\text{physical wave} = \text{Re}(\vec{E}_{\text{total}}) = E_0 \hat{x} (\cos(kz-wt) - \cos(kz+wt))$$

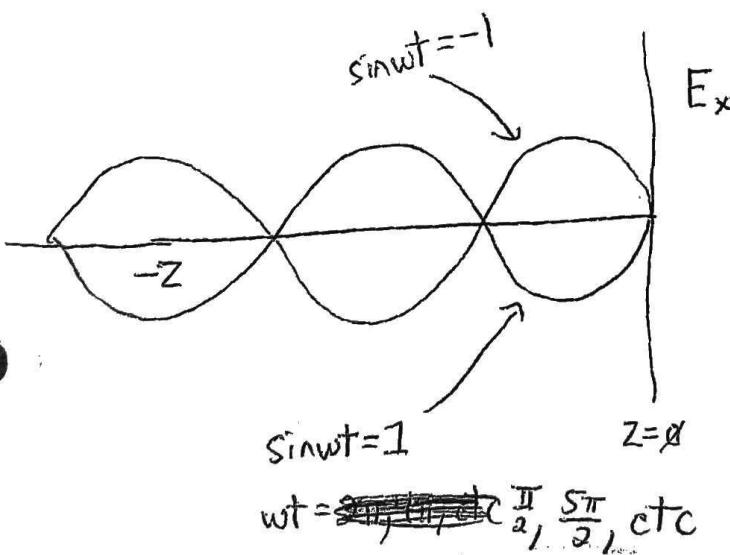
$$\cos(a \pm b) = \cos a \cos b \mp \sin a \sin b$$

$$\Rightarrow E_0 \hat{x} (\cos kz \cos wt + \sin kz \sin wt - (\cos kz \cos wt - \sin kz \sin wt))$$

$$\rightarrow \boxed{\vec{E}_{\text{Final}} = 2E_0 \sin kz \sin wt \hat{x}}$$

standing wave/no node at  
the boundary ( $z=0$ ) since  
 $E, E''$  differ in phase by  $\pi$

the vacuum exists for  $z < 0$  so



and naturally in the  
good conductor limit,  
there is no field  
for  $z > 0$

$$\hat{n} \cdot (\vec{D}_2 - \vec{D}_1) = 0 \quad \hat{n} \cdot (\vec{E}_o' - (\vec{E}_o + \vec{E}_o'')) = 0$$

$\vec{E}_o' = \emptyset$  since its an ideal conductor  $\vec{E}_o + \vec{E}_o'' \cdot \hat{n} = \emptyset$

since  $E$  in  $\hat{x}$  and  $\hat{n}$  is  $\hat{z}$   $\rightarrow \underline{\sigma = \emptyset}$

(no normal component on either side of interface)

$$\hat{n} \times (\vec{H}_2 - \vec{H}_1) = \vec{K}_f \quad \vec{H}_2 = \vec{H}_o' = \emptyset \quad \hat{n} \times (\vec{H}_o + \vec{H}_o'') = -\vec{K}$$

$$\vec{B} = \frac{\vec{K} \times \vec{E}}{\omega} \text{ so } \vec{H} = \frac{1}{\omega \mu} \vec{K} \times \vec{E} \quad \vec{H}_o = \frac{K}{\omega \mu} \hat{z} \times E_o e^{i(kz-wt)} \hat{x}$$

$$\vec{H}_o'' = \frac{K}{\omega \mu} (-\hat{z}) \times (-E_o) e^{i(kz-wt)} \hat{x} = \frac{KE_o}{\omega \mu} e^{i(kz-wt)} \hat{y} = \sqrt{\epsilon} E_o e^{i(kz-wt)} \hat{y}$$

$$= \sqrt{\epsilon} E_o e^{i(kz-wt)} \hat{y} \quad \text{Re}(\vec{H}_o + \vec{H}_o'') = 2\sqrt{\epsilon} E_o e^{i(kz-wt)} \hat{y} \cos(kz)$$

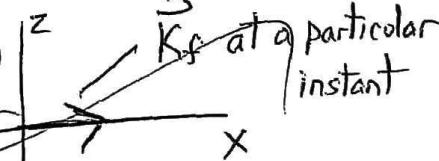
$$\cos \hat{y} \times 2\sqrt{\epsilon} E_o e^{i(kz-wt)} \hat{y} = K_f \quad 2\sqrt{\epsilon} E_o e^{i(kz-wt)} \hat{z} \times \hat{z} = -K_f$$

$$\rightarrow K_f = 2\sqrt{\epsilon} E_o e^{i(kz-wt)} \hat{x}$$

$$\rightarrow K_f = 2\sqrt{\epsilon} E_o \cos(wt) \hat{x}$$

now take the real part and set  $z = \emptyset$

see correction on next page



at that instant,  $\vec{H}$  is clearly in  $\hat{x}$  for  $z < \emptyset$  so its consistent. And then  $\vec{H}$ ,  $\vec{K}$  oscillate in time.

\* so  $\vec{H}_o'' = \vec{H}_o$ , they must be the same.  $\vec{E}$  flipped in phase by  $\pi$  so  $\vec{H}$  couldn't flip or  $\vec{S}$  would be in the wrong direction

correction  $\vec{n} \times (\vec{H}_o + \vec{H}_o'') = -\vec{K}_f$

$$\vec{H}_o + \vec{H}_o'' = \left[ \sqrt{\frac{\epsilon}{\mu}} E_o e^{i(kz-wt)} + \sqrt{\frac{\epsilon}{\mu}} E_o e^{-i(kz+wt)} \right] \hat{y}$$

now  $z=0$  so  $\vec{H}_o + \vec{H}_o'' = \sqrt{\frac{\epsilon}{\mu}} E_o \left[ e^{-iwt} + e^{-iwt} \right] \hat{y}$

since we want the real  $\vec{K}_f$ ,  
lets take  $R_c(\vec{H}_o + \vec{H}_o'')$   $= 2\sqrt{\frac{\epsilon}{\mu}} E_o \cos wt \hat{y}$

$$\hat{n} \times 2\sqrt{\frac{\epsilon}{\mu}} E_o \cos wt \hat{y} = 2\sqrt{\frac{\epsilon}{\mu}} E_o \cos wt \hat{z} \times \hat{y} = -\vec{K}_f$$

$$\Rightarrow \vec{K}_f = \underline{2\sqrt{\frac{\epsilon}{\mu}} E_o \cos wt \hat{x}}$$

at the instant shown,

$\vec{H}$  is clearly in  $\hat{y}$

for  $z < 0$  - so it's consistent

(And then  $\vec{H}$  and  $\vec{K}_f$  oscillate in time)

